

Output tracking

2 versions:

- 1) exact output tracking
- 2) asymptotic output tracking

Exact output tracking

- also called system inversion
- related (but not identical) to different. fl. ta.

Assume that instead of $y(t) \equiv 0$ we want the system to follow (exactly) a given output trajectory $y_d(t)$ -

-> Must find $x(t)$ and $u(t)$ s.t. the system output coincides with $y_d(t)$ -

In the normal form:

$$y_d(t) = \xi_1(t) \quad \forall t \quad \text{hence for all deriv.}$$

$$\xi_2(t) = \dot{y}_d(t)$$

$$\xi_3(t) = y_d^{(n-1)}(t)$$

$$v(t) = y_d^{(n)}(t)$$

which in the original basis corresponds to 1204

$$u(t) = -L_f^r h(\Phi^{-1}(\xi, \eta)) + y_d^{(r)}(t)$$

$$L_g L_f^{r-1} h(\Phi^{-1}(\xi, \eta))$$

call $\underline{y}_d(t) \triangleq \begin{bmatrix} y_d(t) \\ \vdots \\ y_d^{(r-1)}(t) \end{bmatrix}$

For the η variables it is then

$$\dot{\eta} = q(\underline{y}_d(t), \eta)$$

$\eta(0)$ still free

\uparrow
this is now given, time-dependent profile

~~Drawback~~ Drawback of exact tracking: need to ~~know~~ preset the initial conditions of the system, i.e. to fix $\xi(0)$

→ more realistic to ask to track the output asymptotically

Asymptotic output tracking

Given the system in normal form

$$\dot{\xi} = A\xi + Bv$$

$$\dot{\eta} = q(\xi, \eta)$$

$$y = [1 \ 0 \ \dots \ 0] \xi$$

and a reference output $y_d(t)$

Consider the output tracking error

$$e(t) = y(t) - y_d(t)$$

exact tracking corresponds to $e(t) = 0 \forall t$

since $\xi_{i+1} = y^{(i)} = L_f^i h(x)$

$$e^{(i)}(t) = y^{(i)} - y_d^{(i)} = L_f^i h(x) - y_d^{(i)} \quad i=0,1,\dots,r-1$$

we can replace ξ with the error vector

$$E = \begin{bmatrix} e_1 \\ \vdots \\ e_r \end{bmatrix} \stackrel{\Delta}{=} \begin{bmatrix} e \\ \dot{e} \\ \vdots \\ e^{(r-1)} \end{bmatrix} = \begin{bmatrix} \xi_1 - y_d \\ \xi_2 - \dot{y}_d \\ \vdots \\ \xi_r - y_d^{(r-1)} \end{bmatrix}$$

$$\Rightarrow \dot{E} = \begin{bmatrix} 0 & 1 & & \\ & 0 & \ddots & \\ & & \ddots & 0 \\ 0 & & & 0 \end{bmatrix} E + \begin{bmatrix} 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} v$$

new state (error)

$$\dot{\eta} = q(E, \eta) = q(E + \gamma_d(t), \eta)$$

η unchanged

$$e(t) = e_1(t)$$

new output (error)

the equiv. of zero dynamics for this system is now when $E(t) = 0$

i.e. it is $\dot{\eta} = q(\gamma_d(t), \eta)$

this is however time-varying, hence its stability must be in a uniform sense!

thm Assume $\gamma_d(t)$ are defined and bounded

$\forall t$ - Let η_d be the solution of

$$\dot{\eta} = g(\gamma_d(t), \eta) \quad (\text{i.e. in corresp. of } f(t) \equiv 0 \rightarrow \text{zero dyn.})$$

Suppose this solution is bounded and uniformly asympt. stable -

Then for $\eta(0)$ near $\eta_d(0)$ and for $\epsilon(0)$ small
~~∃~~ a feedback $v = K\epsilon$ s.t. $A+BK$ Hurwitz
~~is s.t.~~ $\epsilon(t) \xrightarrow{t \rightarrow \infty} 0$ and η bounded -

meaning: bounded tracking is achieved

- $\epsilon(t) \rightarrow 0$
- η stays bounded

Disturbance decoupling problem

(17207)

Consider a ^{SISO} system with an additive disturbance w

$$\begin{aligned}\dot{x} &= f(x) + g(x)u + p(x)w \\ y &= h(x)\end{aligned}$$

$p(x)$ = vect. field of the disturbance

Problem (disturbance decoupling)

~~Find α & β~~ Under what conditions \exists a feedback law $u = \alpha(x) + \beta(x)v$ s.t. the disturbance w has no effect on the output y ?

thm The disturbance decoupling problem is solvable iff

$$L_p L_f^k h(x) = 0 \quad k = 0, 1, \dots, r-1$$

where r = rel. degree of the system.

Proof revisit the transformation into normal form

$\xi_1 = y = h(x)$ is not affected by w

$$\dot{y} = \frac{\partial h}{\partial x} (f(x) + g(x)u + p(x)w)$$

$$= L_f h(x) + \underbrace{L_g h(x)u}_{=0} + \underbrace{L_p h(x)w}_{=0}$$

if $r > 1$
 $\Rightarrow w$ does not appear in $\dot{y} = \dot{s}_2$

$$y^{(r)} = L_f^r h(x) + \underbrace{L_g L_f^{r-1} h(x)u}_{\neq 0} + \underbrace{L_p L_f^{r-1} h(x)w}_{=0}$$

\Rightarrow with the usual choice of input

$$u(x) = \frac{-L_f^r h(x) + v}{L_g L_f^{r-1} h(x)}$$

also $y^{(r)} = \dot{s}_r = v$ is not affected by w

\Rightarrow normal form

$$\begin{cases} \dot{s}_1 = s_2 \\ \vdots \\ \dot{s}_{r-1} = s_r \\ \dot{s}_r = v \\ \dot{\eta} = q(s, \eta, w) \\ y = s_1 \end{cases}$$

\Rightarrow disturbance is decoupled from output;
only zero dynamics is affected (unobservable)

- Meaning: the relative degree $w \rightarrow y$ has to be strictly bigger than the rel. degree $u \rightarrow y$
- Geometrically:

$$p(x) \perp \text{span} \left\{ \frac{\partial h}{\partial x}, \frac{\partial (L_f h)}{\partial x}, \dots, \frac{\partial (L_f^{r-1} h)}{\partial x} \right\}$$

CONTROL LYAPUNOV FUNCTIONS

h209

Consider the system

$$\dot{x} = f(x) + g(x)u$$

$$\text{at } x_0 = 0$$

$$(s.t. f(0) = 0)$$

Problem: want to find (static) state feedback law $u = \psi(x)$ s.t. the closed loop is

$$\dot{x} = f(x) + g(x)\psi(x)$$

is (locally or globally) asymptotically stable at x_0 .

From a converse Lyapunov theorem: if x_0 is (locally or globally) asymptotically stable \Rightarrow

\exists a Lyapunov function $V > 0$ s.t.

$$\dot{V}(x) = \frac{\partial V}{\partial x} (f(x) + g(x)\psi(x)) < 0$$

or $\dot{V}(x) < -W(x)$ with $W(x) > 0$ if we

want a certain rate of convergence

(for instance exponential if $W(x) \sim \|x\|$)

def $V > 0$, C^1 is a (local or global) Control Lyapunov Function (CLF) if for some $u \in \mathbb{R}$

$$\frac{\partial V}{\partial x} (f(x) + g(x)u) < 0 \quad \text{for } x \neq 0$$

(locally or globally around $x_0 = 0$)

Consequences:

- 1) $\dot{V} < 0 \Rightarrow$ when $L_g V(x) = \frac{\partial V}{\partial x} g(x) = 0$ then it must be $L_f V(x) = \frac{\partial V}{\partial x} f(x) < 0$

meaning: drift must be asymptotically stable when the control part cannot compensate for it

- 2) If we want $u = \psi(x)$ continuous (so that the closed-loop system is continuous) $\psi(0) = 0$, then V has the small control prop.

def V has the small control property if $\forall \epsilon > 0 \exists \delta > 0$ s.t. if $x \neq 0$ and $\|x\| < \delta$ then $\exists u$ with $\|u\| < \epsilon$ s.t. $L_f V(x) + L_g V(x)u < 0$

(u211)

measuring $\dot{V} < 0$ cannot be guaranteed by blowing the control amplitude when $\|x\| \rightarrow 0$ (if so you get discontinuous behavior at $x=0$).

• How to choose $u = \psi(x)$?

For instance try "canceling" the dynamics

$$u = \psi(x) = \begin{cases} \frac{-L_f V(x) + \gamma(x)}{L_g V(x)} & \text{when } L_g V(x) \neq 0 \\ \text{anything} & \text{when } L_g V(x) = 0 \end{cases}$$

$$\Rightarrow \dot{V} = \cancel{L_f V(x)} + L_g V(x) \left(\frac{-\cancel{L_f V(x)} + \gamma(x)}{\cancel{L_g V(x)}} \right) = \gamma(x)$$

for $L_g V(x) \neq 0$

Difficulty: choose $\gamma(x)$ so that $u = \psi(x)$ is continuous and $\dot{V}(x) < 0 \ \forall x$
 ($\gamma(x)$ must be < 0 for $L_g V(x) \neq 0$)

when the small control property holds then there is a constructive formula, called universal Sontag formula

thm let V be a (local or global) CLF and assume the small control property holds - then the origin is (locally or globally) stabilizable by the feedback $u = \psi(x)$ where

$$\psi(x) = \begin{cases} - \frac{L_f V(x) + \sqrt{(L_f V(x))^2 + (L_g V(x))^2}}{L_g V(x)} & \text{if } L_g V(x) \neq 0 \\ 0 & \text{if } L_g V(x) = 0 \end{cases}$$

Proof

• If $L_g V(x) = 0 \Rightarrow \dot{V} = L_f V(x) < 0$ for $x \neq 0$ by def. of CLF

• If $L_g V(x) \neq 0$

$$\begin{aligned} \dot{V} &= \cancel{L_f V(x)} - \cancel{L_g V(x)} \frac{(\cancel{L_f V(x)} + \sqrt{(L_f V)^2 + (L_g V)^2}}{\cancel{L_g V(x)}} \\ &= - \sqrt{(L_f V)^2 + (L_g V)^2} < 0 \end{aligned}$$

• If $L_g V(x) = 0$ then $\dot{V} = L_f V < 0$ by def of CLF

- consequence: \exists of a CLF is necessary and sufficient for (local or global) stabilization.
- Difficulty: a CLF must be given!
- How to find a CLF? If you have any method that stabilizes the system then you ~~have~~ also get a CLF (but it could not be easy to find V for a as. stable closed loop system ...)

example: $\dot{x} = ax - bx^3 + u$ $a, b > 0$

from feedback linearization:

$$u = -ax + bx^3 - kx \quad k > 0$$

leads to the closed loop system

$$\dot{x} = -kx$$

which is globally as. (exp.) stable and has $V(x) = \frac{1}{2}x^2$ as Lyapunov funct. (radially unbounded)

let us compute Sontag formula:

$$L_g V(x) = \frac{\partial V(x)}{\partial x} g = x$$

$$L_f V(x) = \frac{\partial V}{\partial x} f = x(2x - bx^3)$$

in x s.t. $L_g V \neq 0$ (i.e. for $x \neq 0$)

$$\Rightarrow u = \psi(x) = \frac{-L_f V + \sqrt{(L_f V)^2 + (L_g V)^4}}{L_g V}$$

$$= \frac{-x(2x - bx^3) + \sqrt{x^2(2x - bx^3)^2 + x^4}}{x}$$

$$= -2x + bx^3 - x\sqrt{(2 - bx^2)^2 + 1}$$

compare this feedback with the feedback
Emulating u

$$u = -2x + bx^3 - kx$$

• Sontag formula has a robustness w.r.t. the input amplitude: replacing $u = \psi(x)$ with $u = k\psi(x)$ $k > \frac{1}{2}$ stabilization property is preserved.

• meaning of the formula: it guarantees sufficient smoothness to $\psi(x)$