

Evaluation of Six Different Sensor Fusion Methods for an Industrial Robot using Experimental Data



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1. Introduction

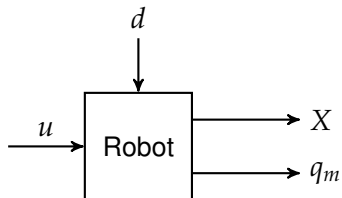
- Problem Formulation
- Bayesian Estimation

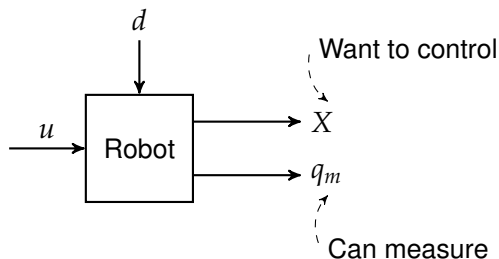
2. Modelling

- Robot Model
- Accelerometer Model
- Estimation Models

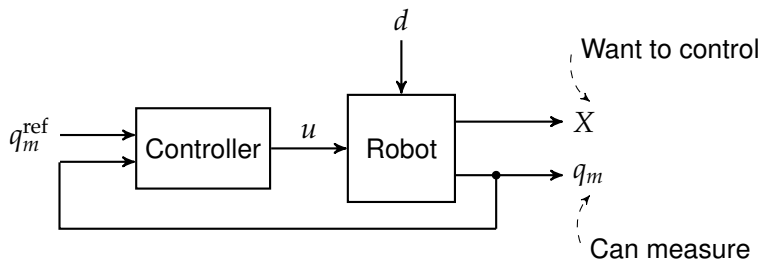
3. Experimental Results



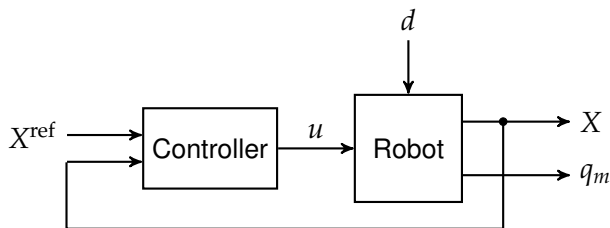




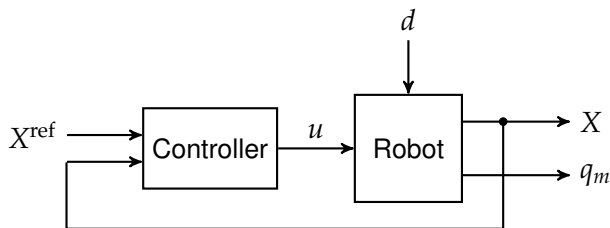
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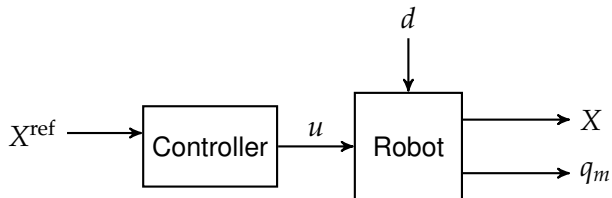
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- If the TCP can be measured it is natural to feedback it.

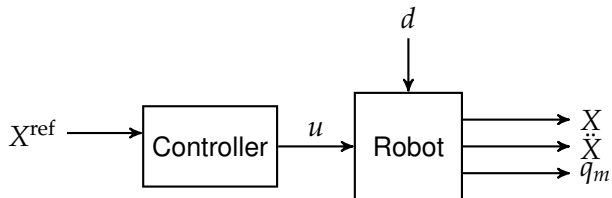


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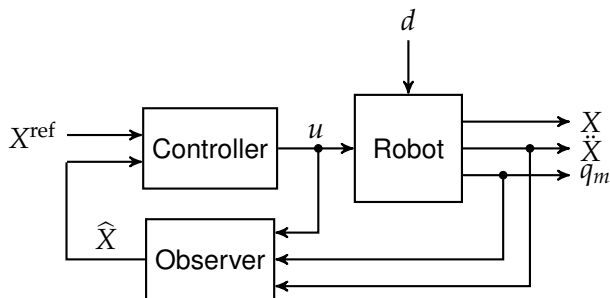
What can we do instead of measuring the TCP?



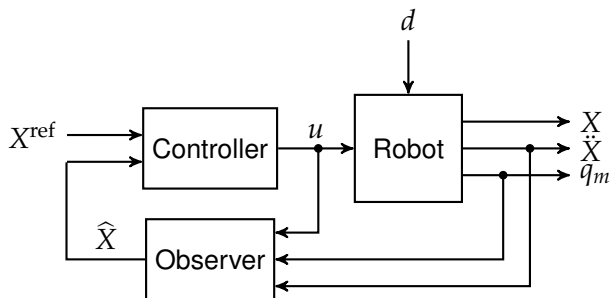




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How can we estimate the TCP?

Model:

$$\begin{aligned}x_{k+1} &= f(x_k, u_k, w_k), \\ y_k &= h(x_k) + e_k.\end{aligned}$$

Bayesian inference:

$$\begin{aligned}p(x_{k+1}|y_{1:k}) &= \int_{\mathbb{R}^n} p(x_{k+1}|x_k)p(x_k|y_{1:k}) dx_k, \\ p(x_k|y_{1:k}) &= \frac{p(y_k|x_k)p(x_k|y_{1:k-1})}{p(y_k|y_{1:k-1})}.\end{aligned}$$

- The Kalman filter is the optimal choice for linear models.
- Approximative filters have to be used for nonlinear models.



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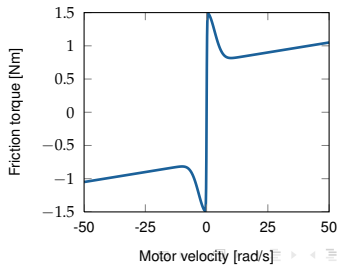
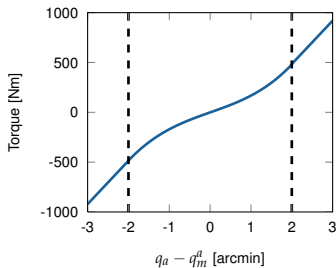
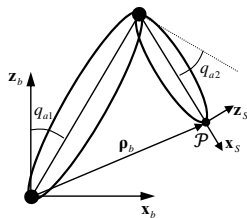
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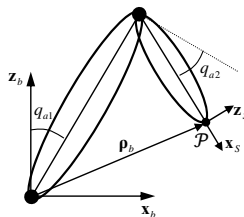
- The Kalman filter is the optimal choice for linear models.
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- In this work:
 - Extended Kalman filter (EKF) (Extended Kalman smoother (EKS))
 - Approximate the system with a linearisation of the nonlinear equations.
 - Assume additive Gaussian noise.
 - Particle filter (PF)
 - Approximate the posterior distribution with a large number of particles.
 - The optimal proposal distribution approximated using an EKF.



- Serial robot with 2 DOF.
- Nonlinear stiffness.
- Nonlinear friction.



- Acceleration from the motion.
- Acceleration due to the gravity.
- Rotation matrix from Ox_bz_b to Ox_sz_s .
- Bias parameter.



$$\ddot{\rho}_s(q_a) = \mathcal{R}_{b/s}(q_a) (\ddot{\rho}_b(q_a) + G_b) + \mathbf{b}^{\text{ACC}}$$

1. Nonlinear estimation model

- State space vector:

$$x = (x_1^T \quad x_2^T \quad x_3^T \quad x_4^T)^T = (q_a^T \quad q_m^{a,T} \quad \dot{q}_a^T \quad \dot{q}_m^{a,T})^T$$

- Physical model gives a continuous-time state space model.
- Discretisation using Euler sampling gives

$$x_{k+1} = f(x_k, u_k) + g(x_k)v_k.$$



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- Measurement equation:

$$y_k = \left(\mathcal{R}_{b/s}(x_{1,k}) \left(J_{\text{ACC}}(x_{1,k}) \overset{x_{2,k}}{\ddot{q}_{a,k}} + \left(\frac{d}{dt} J_{\text{ACC}}(x_{1,k}) \right) x_{3,k} + G_b \right) \right) + e_k$$



2. Estimation model with linear dynamic

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$$x = (x_1^T \quad x_2^T \quad x_3^T)^T = (q_a^T \quad \dot{q}_a^T \quad \ddot{q}_a^T)^T$$

- Linear dynamic model (Double integrator in discrete time):

$$x_{k+1} = \mathcal{F}x_k + \mathcal{G}_u u_k + \mathcal{G}_v v_k$$

- The input signal is the jerk of the arm angle reference.



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- Measurement equation:

$$y_k = \begin{pmatrix} x_{1,k} + K^{-1} (M_a(x_{1,k})x_{3,k} + C(x_{1,k}, x_{2,k}) + G(x_{1,k})) \\ \mathcal{R}_{b/s}(x_{1,k}) \left(J_{ACC}(x_{1,k})x_{3,k} + \left(\frac{d}{dt} J_{ACC}(x_{1,k}) \right) x_{2,k} + G_b \right) \end{pmatrix} + e_k$$



3. Nonlinear estimation model with acceleration as input

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- Arm angular acceleration calculated from the accelerometer signal.
- The physical model + Euler sampling give

$$x_{k+1} = \begin{pmatrix} x_{1,k} + T_s x_{3,k} \\ x_{2,k} + T_s x_{4,k} \\ x_{3,k} + T_s \ddot{q}_{a,k}^{IN} \\ x_{4,k} + T_s M_m^{-1} (u_k - F(x_{4,k}) + T(x_{1,k} - x_{2,k}) + D(x_{3,k} - x_{4,k})) \end{pmatrix} + g(x_k) v_k.$$



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$$y_k = (\mathbf{0} \quad \mathbf{I} \quad \mathbf{0} \quad \mathbf{0}) x_k + e_k$$



4. Linear estimation model with acceleration as input

- State space vector:

$$x = (x_1^T \quad x_2^T \quad x_3^T \quad x_4^T)^T = (q_a^T \quad q_m^{a,T} \quad \dot{q}_a^T \quad \dot{q}_m^{a,T})^T$$

- Arm angular acceleration calculated from the accelerometer signal.
- The physical model + Linear spring, damper and friction give

$$\dot{x} = \begin{pmatrix} \mathbf{0} & \mathbf{0} & \mathbf{I} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ M_m^{-1}K & -M_m^{-1}K & M_m^{-1}D & -M_m^{-1}(D + F_d) \end{pmatrix} x + \begin{pmatrix} \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \\ \mathbf{I} & \mathbf{0} \\ \mathbf{0} & M_m^{-1} \end{pmatrix} \begin{pmatrix} \ddot{q}_a^{\text{IN}} \\ u \end{pmatrix}.$$

- Discretisation using ZOH.



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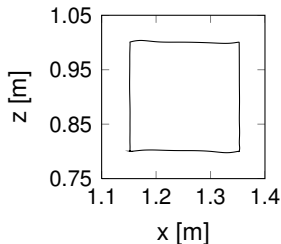
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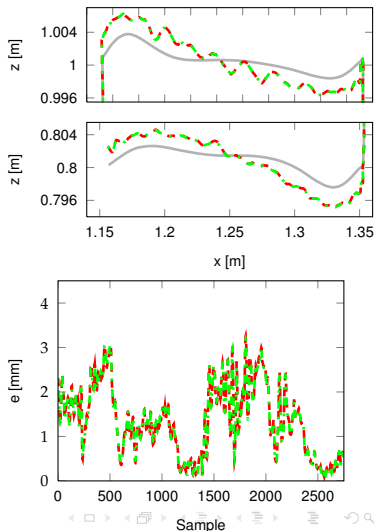
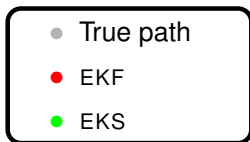
- Experiments performed on an ABB IRB4600.
- Only joints 2 and 3 are used.
- The true path is measured by a laser system from Leica.
- Synchronization errors and kinematic errors are present.



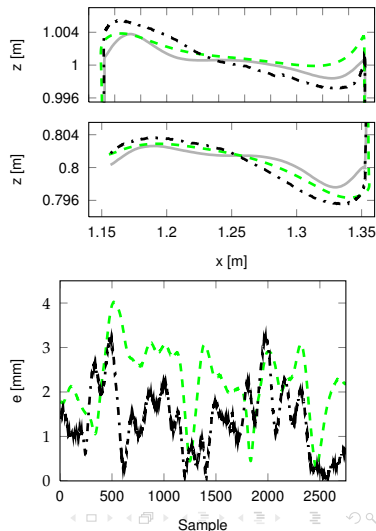
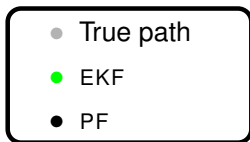
Calibration of the accelerometer: Patrik Axelsson and Mikael Norrlöf, **Method to Estimate the Position and Orientation of a Triaxial Accelerometer Mounted to an Industrial Manipulator**. In proceedings of the 10th International IFAC Symposium on Robot Control, 2012.



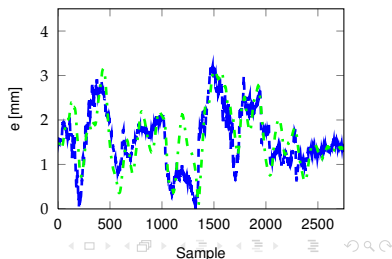
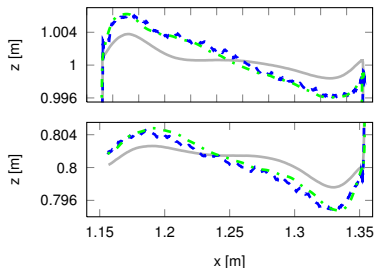
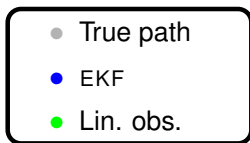
- Gives the same estimation.
- Higher orders of oscillation in the estimated paths.
- Bias states does not affect the result.
- The current MATLAB implementation not in real-time for the observers.



- Both filters follow the true path.
- The EKF passes in the corners.
- Bias states for both motor and accelerometer measurements are required to get good results.
- The current MATLAB implementation not in real-time for the observers.



- Linear model and pole placement works fine.
- Nonlinear model and EKF has higher orders of oscillations.
- No bias compensation.
- The current MATLAB implementation in real-time for the observers.



- EKF + Model 1, PF + Model 2, and EKF + Model 3 are the best.
- Complexity: (Models and implementation)
 - EKF + Model 1 Much time spent on modelling.
 - PF + Model 2 Simpler modelling but more difficult to implement.
 - EKF + Model 3 Nonlinear joint model, no rigid body modelling.



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- Computation time:
 - EKF + Model 1 Probably real-time with better implementation.
 - PF + Model 2 Far from real-time.
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- Computation time:
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 - EKF + Model 3 Real-time.
- Robustness:
 - EKF + Model 3 No rigid body parameters.
- Other:
 - PF + Model 2 Entire distribution of the states given. Used for e.g. control and diagnosis!?



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